LA-UR-12-23668

Approved for public release; distribution is unlimited.

Title: Bulk Nanolayered Composites: Interfacial Influence on Microstructural

Evolution at Large Plastic Strains

Author(s): Mara, Nathan A.

Carpenter, John S. Han, Weizhong Zheng, Shijian McCabe, Rodney J.

Wang, Jian

Beyerlein, Irene J.

Intended for: Microscopy and Microanalysis 2012, 2012-07-29/2012-08-01 (Phoenix,

Arizona, United States)

Invited Talk



Disclaimer:

Los Alamos National Laboratory, an affirmative action/equal opportunity employer,is operated by the Los Alamos National Security, LLC for the National NuclearSecurity Administration of the U.S. Department of Energy under contract DE-AC52-06NA25396. By approving this article, the publisher recognizes that the U.S. Government retains nonexclusive, royalty-free license to publish or reproduce the published form of this contribution, or to allow others to do so, for U.S. Government purposes. Los Alamos National Laboratory requests that the publisher identify this article as work performed under the auspices of the U.S. Departmentof Energy. Los Alamos National Laboratory strongly supports academic freedom and a researcher's right to publish; as an institution, however, the Laboratory does not endorse the viewpoint of a publication or guarantee its technical correctness.

Bulk nanolayered composites: Interfacial influence on microstructural evolution at large plastic strains N.A. Mara

Center for Integrated Nanotechnologies

Los Alamos National Laboratory

Co-Authors:

J. Carpenter, W.Z. Han, S. Zheng, R. McCabe, J. Wang, I.J. Beyerlein











Layered composites: Improving mechanical properties since Egyptian times

Plywood—found in Egyptian tombs dating to 3500 BC



--courtesy Amazon.com





Damascus steel production began ~300BC

Moro barung from Philippines—courtesy Wikipedia

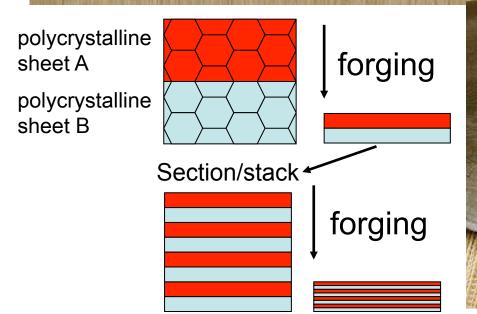




Metallic lamellar composites: Damascus steel



Two different types of steel repeatedly forge-welded together—high strength and toughness combined





Moro barung from Philippines—courtesy Wikipedia





Defects and Interfaces: Interface-driven material behavior

Constituent-dominated behavior

Metal A

Metal B

Low density of interfaces

Phases

Nucleation Storage

Recovery Blocking

Interface
Nucleation
Storage
Recovery
Blocking

Interface-dominated behavior

High density of interfaces





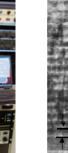
Extraordinary behavior of Physical Vapor Deposited (PVD) multilayers

PVD multilayer fab



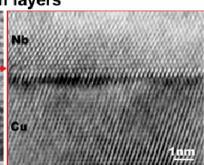
He implantation: resistance to He bubble formation.¹

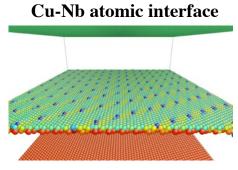
5 nm



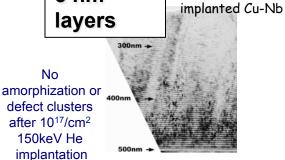
No bubbles in He-

Cu-Nb 2.5 nm layers

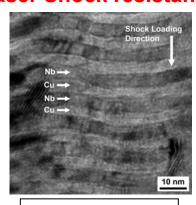




Laser Shock resistance

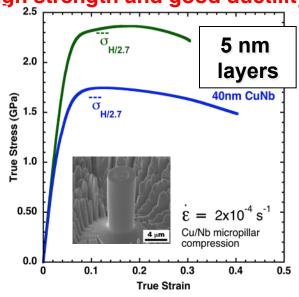


He solubility: ~8%at.



5 nm layers

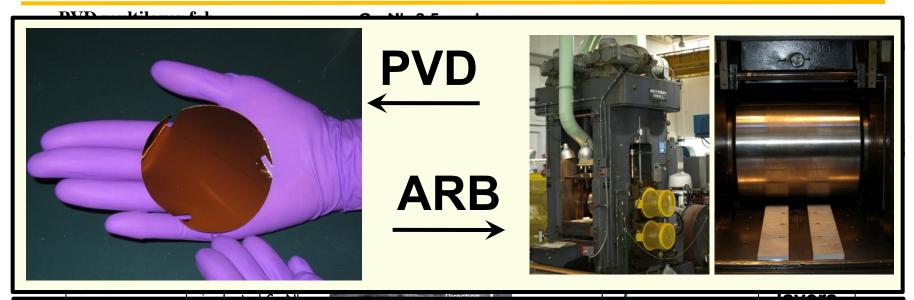
Micropillar Compression: High strength and good ductility²







Extraordinary behavior of Physical Vapor Deposited (PVD) multilayers

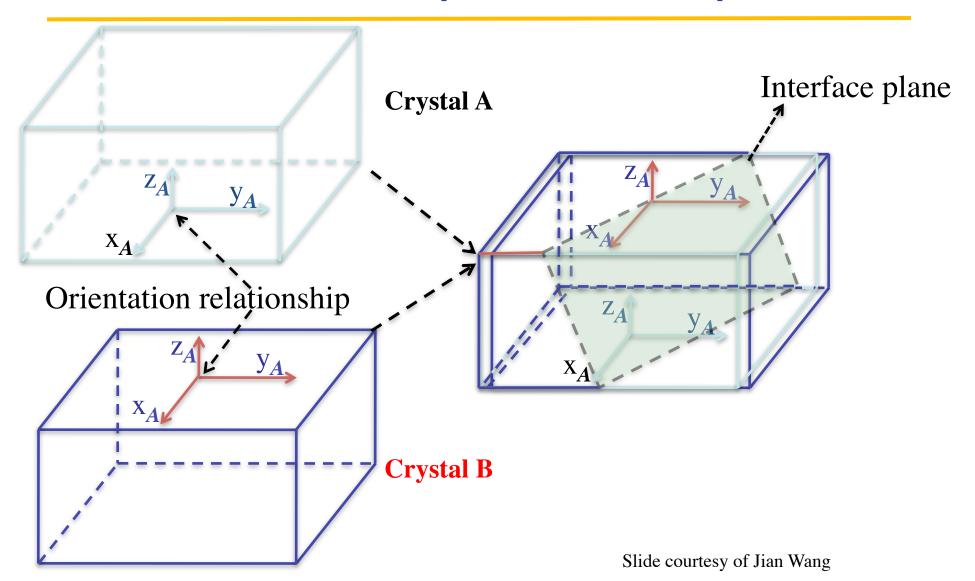


Hypothesis: The atomic structure of an interface dictates its mechanical response. Interfaces with different atomic structure will exhibit different mechanical behavior. Controlling synthesis routes can give preferred interfacial structures with superior properties.





Orientation relationship and interface plane

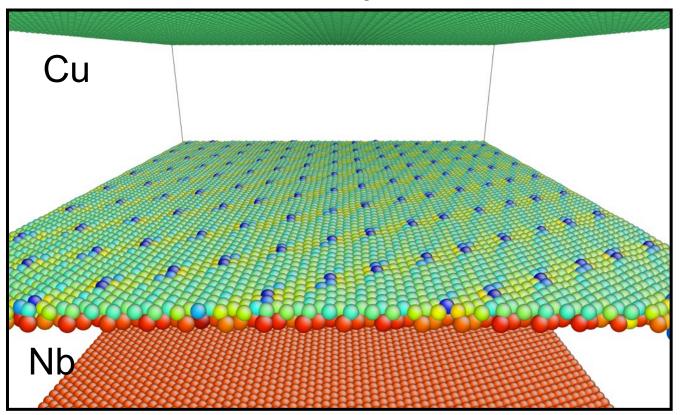






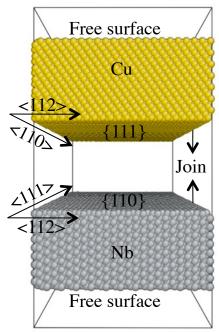
PVD foils: Fine sample dimensions and relatively uniform interfacial properties

Cu-Nb 2.5 nm layers



Characteristic interface in PVD foils

Interface planes: $\{111\}_{Cu} \parallel \{110\}_{Nb}$

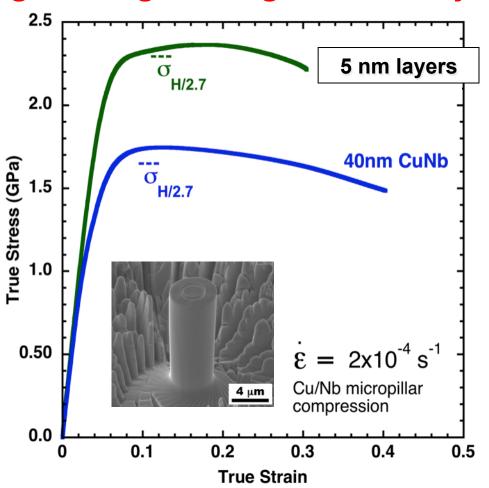






Extraordinary behavior of Physical Vapor Deposited (PVD) multilayers

Micropillar Compression: High strength and good ductility



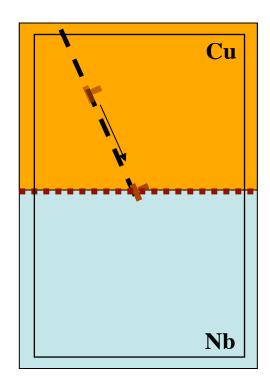
One distinguishing feature makes this material different from pure Cu or Nb

High interfacial content

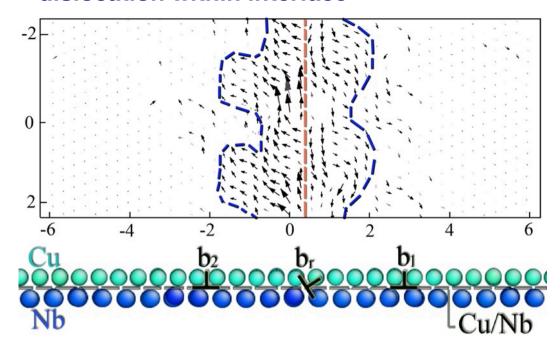
N.A. Mara et al., APL, **92** (2008) 213901. N.A. Mara et al., APL, **97** (2010) 021909.



Glide dislocations are trapped by weak interfaces innovation for our nation that shear in response to dislocation stress field



Core spreading of an edge Shockley partial dislocation within interface



Dashed lines indicate the position while the glide dislocation entering interface.

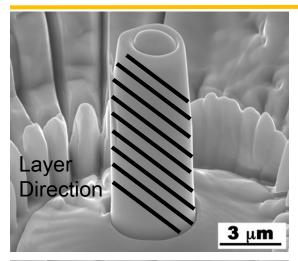
Blue dashed curves outline the region of core spreading within interface.

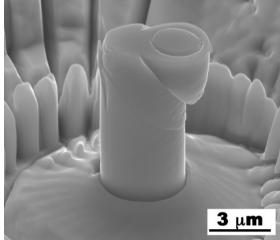
J. Wang, R.G. Hoagland, J.P. Hirth and A. Misra, Acta Materialia (2008).

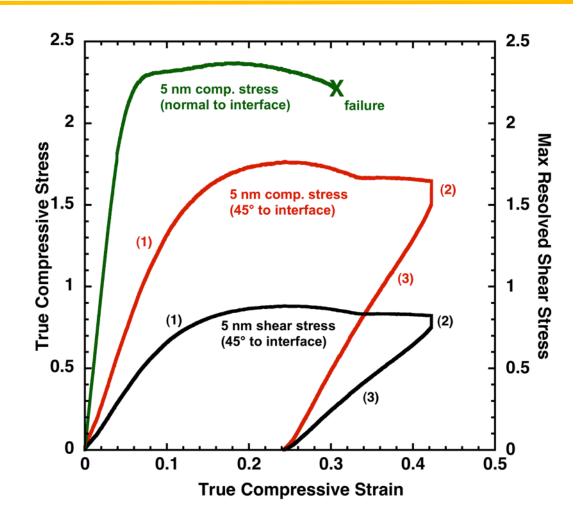




5 nm CuNb multilayers: layer interface oriented 45° w/r to compression axis











Physical Vapor Deposited Cu/Nb--Conclusions

- Atomic structure of the PVD Kurdjumov-Sachs {111}Cu// {110}Nb interface dictates its mechanical behavior
 - Interface is relatively weak in shear
 - Dislocation core spreading in the interface due to low shear strength makes transmission difficult
 - No deformation twinning evident, even after large strains

Questions:

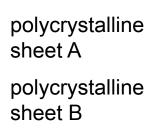
- How will interfaces with differing atomic structure behave under mechanical loading?
- Effects of:
 - Crystal geometry
 - Misfit dislocation structure
 - Synthesis pathway

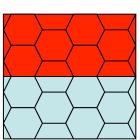


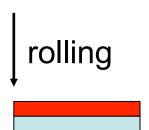
LDRD innovation for our nation

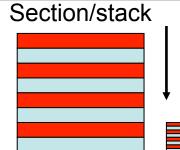
Synthesis of bulk multi-layered nano composite materials chemically identical to PVD

Accumulative Roll Bonding (ARB): Sheet





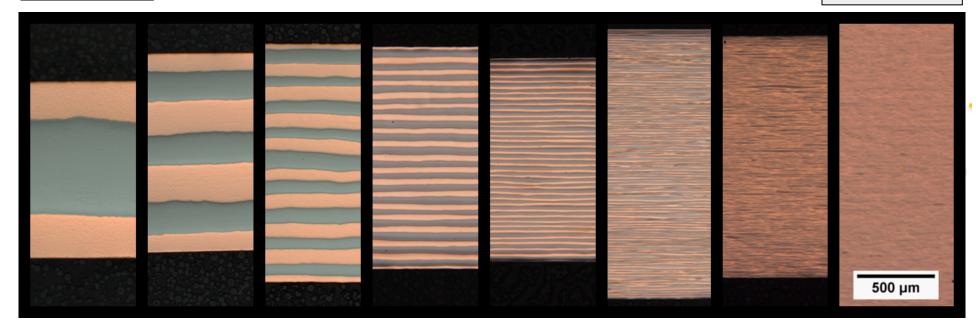




rolling

1-2 mm

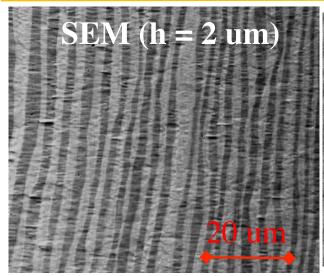
~0.5 µm

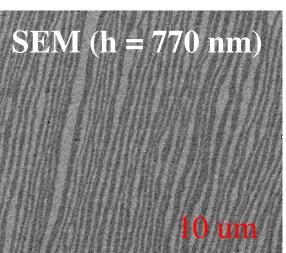


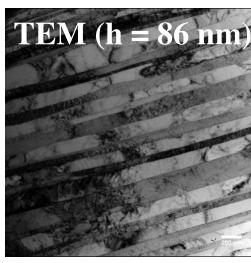




ARB Cu/Nb composites with controllable layer thickness





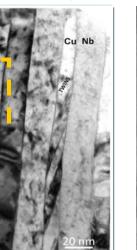


TEM (h = 48 nm)

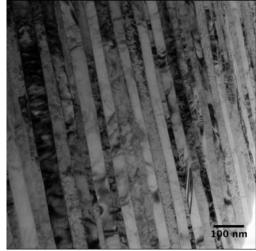
Interface

structure?

TEM (h = 18 nm)



TEM (h = 9 nm)

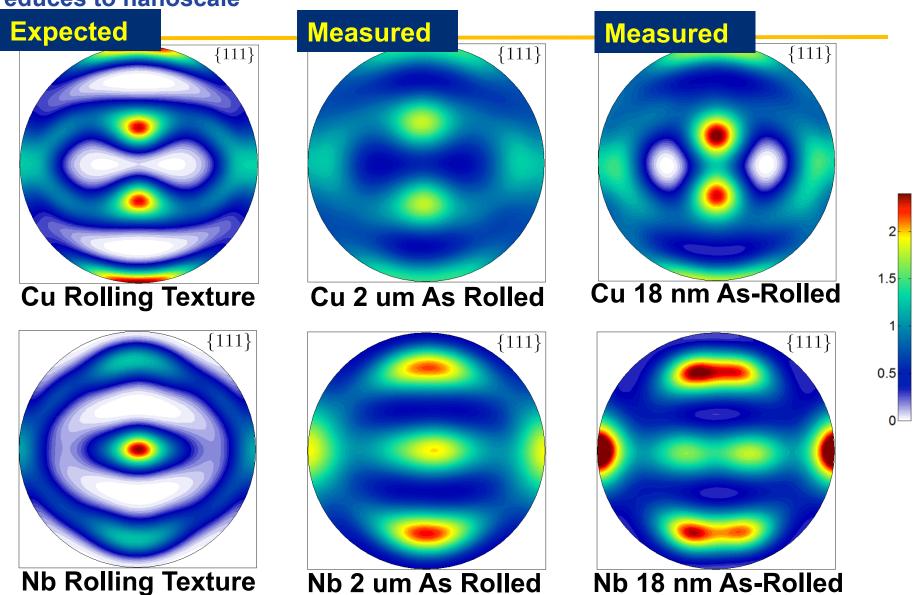


Carpenter et al. 2012, Acta Mater.





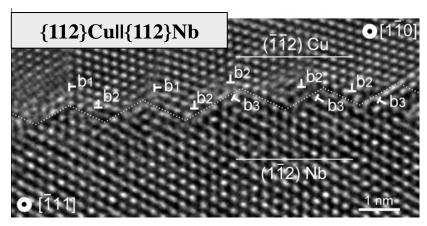
Deviations from theoretical rolling texture as the layer thickness reduces to nanoscale



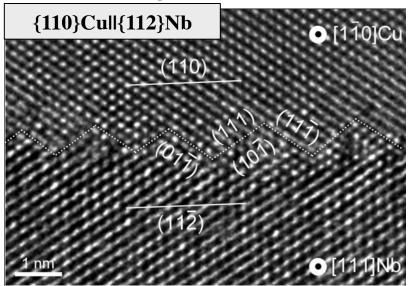




Two interfaces with same KS orientation relationship but different interface planes



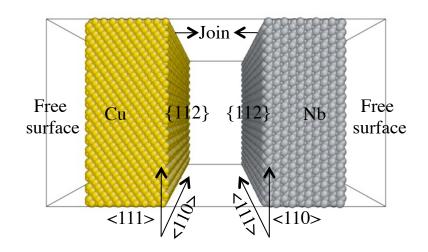
S. J. Zheng et al. 2012, Acta Mater., In Press

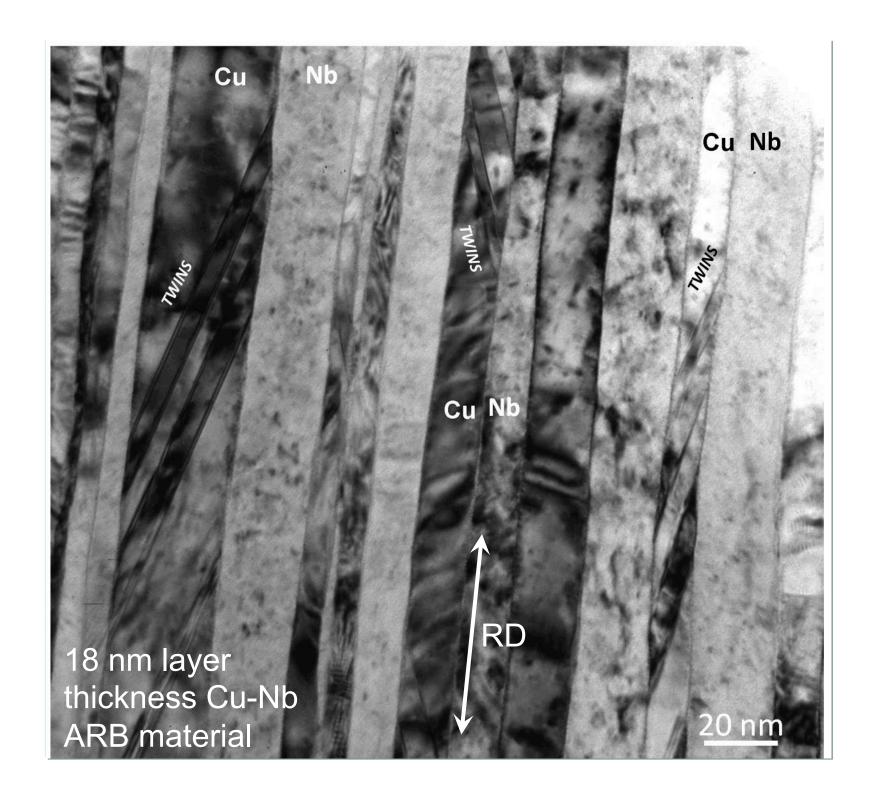


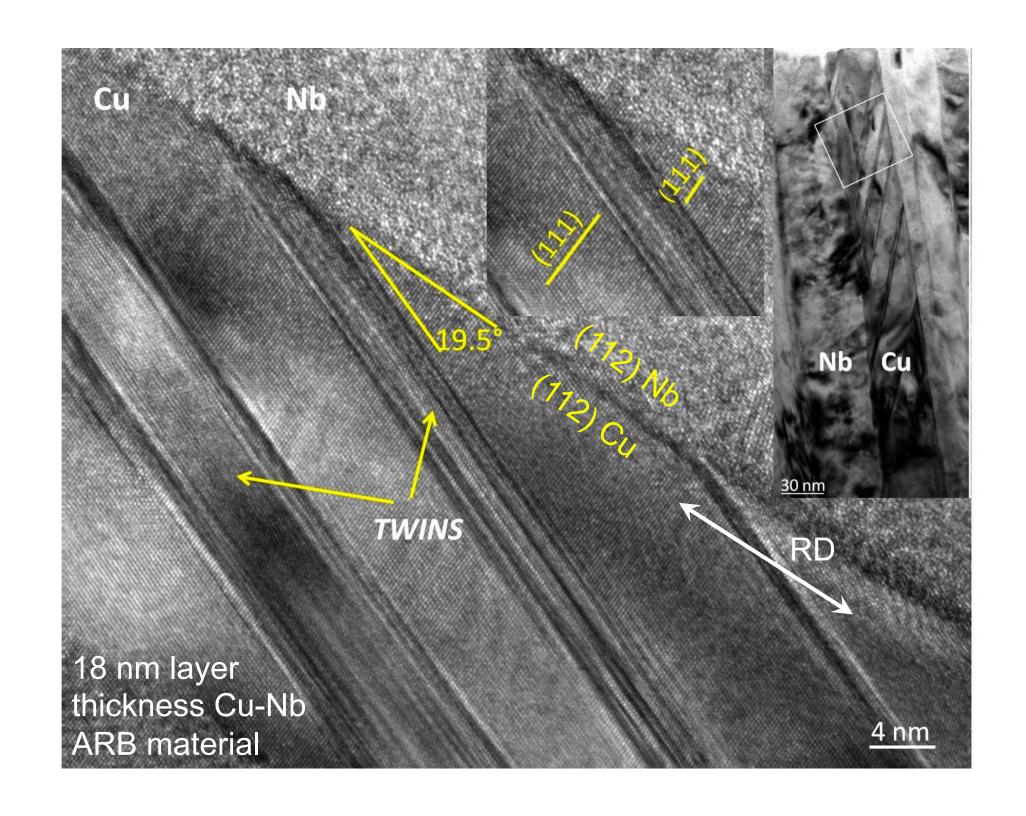
TD|| <110>Cu||<111>Nb

Characteristic interface in fine ARB samples

Interface planes: $\{112\}_{Cu} \parallel \{112\}_{Nb}$



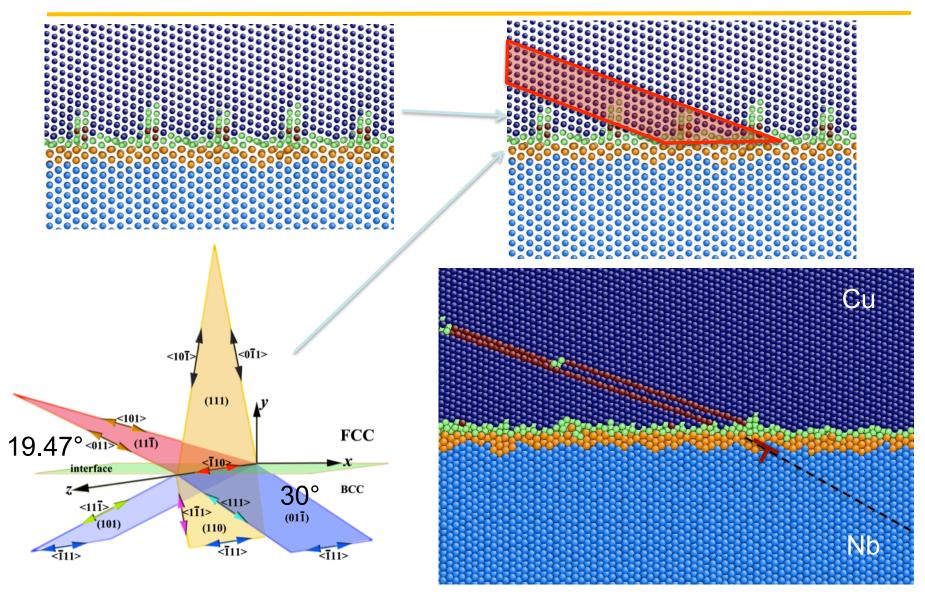








{112}Cu//{112}Nb KS: Twinning is preferred on the (11-1) slip plane



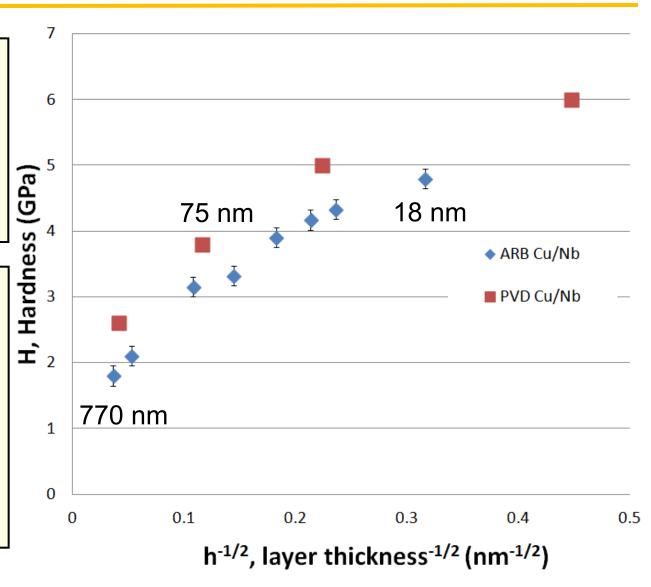




ARB Material Presents Lower Strength as compared to PVD material

Is the ARB interface a less effective barrier to slip than the PVD interface?

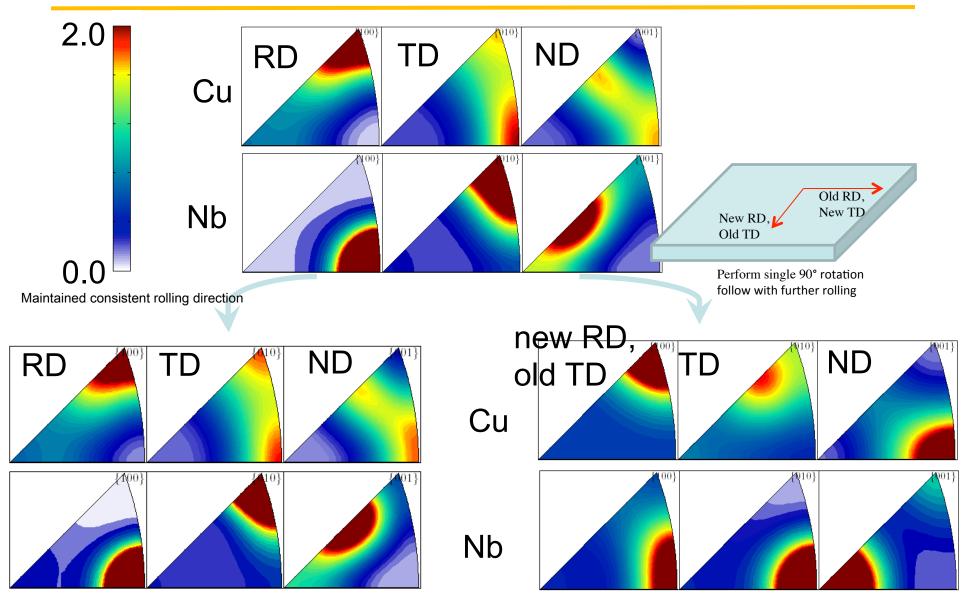
Is the ARB material, with its texture produced via rolling, simply softer in certain directions due to this texture?







90° Strain path change: 56 nm to 30 nm

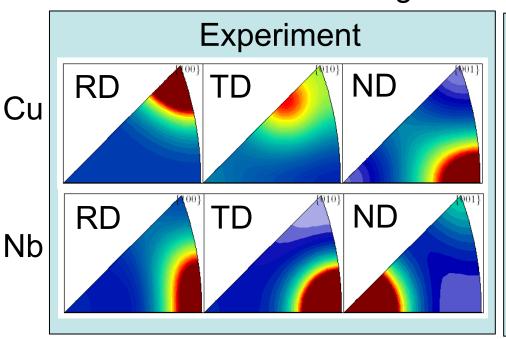


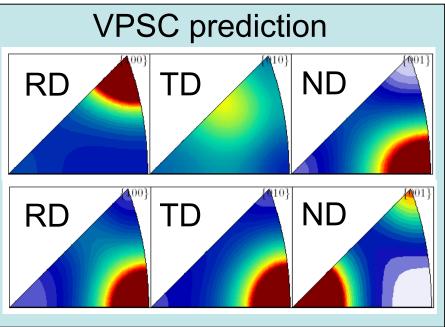




90° Strain path change: 56 nm to 30 nm

Inverse Pole Figures after Strain Path Change





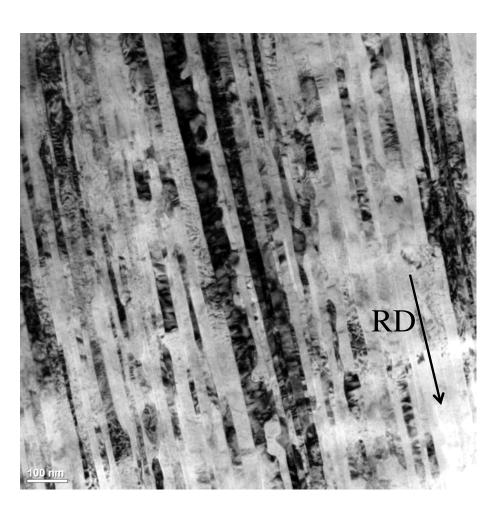
VPSC can predict textures, and can aid in predicting new interface OR/IP



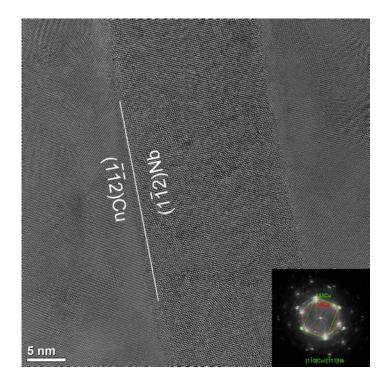




18 nm Cu/Nb Annealed at 500°C



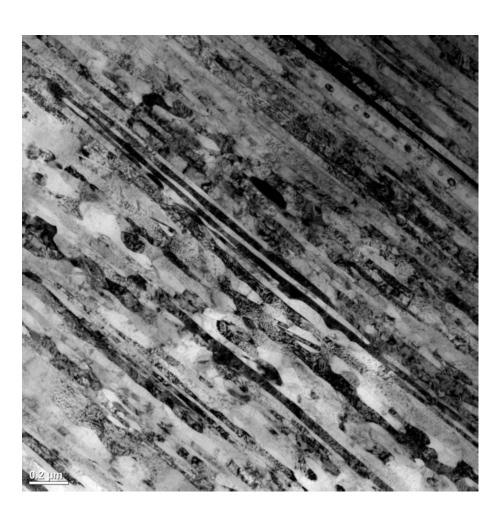
- Layers maintain ~ 18 nm layer thickness
- Interfaces are still largely planar
- Locations do show initial stages of instability, but not at (112)||(112) interfaces



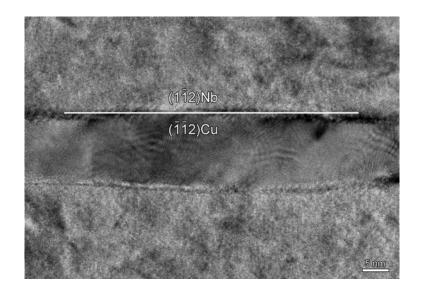




18 nm Cu/Nb Annealed at 600°C



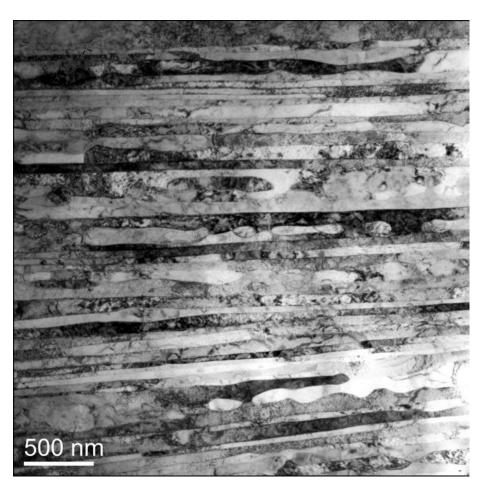
- Layers are becoming noticeably thicker
 50 nm in thickness
- Interfaces are still largely planar
- More instability noted, but not at (112)||
 (112) interfaces

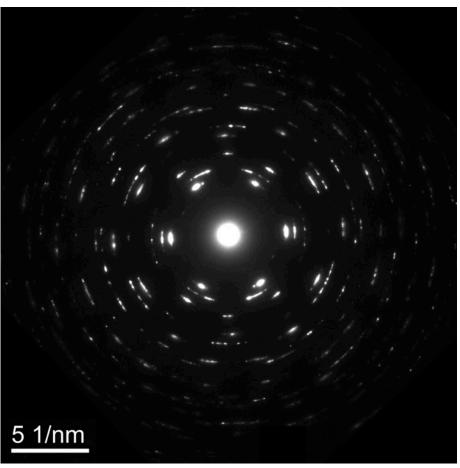






18 nm Cu/Nb Annealed at 700°C



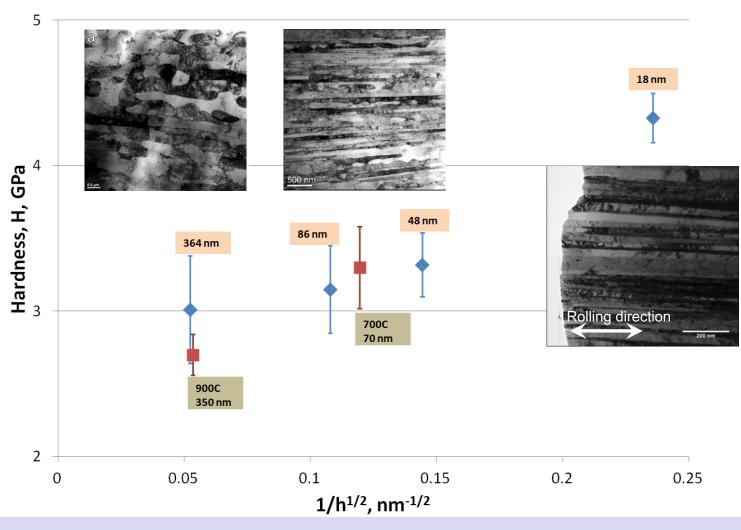


Strong texture and lamellar structure is maintained





Mechanical Behavior – 700C Maintains Strength Trend



Lamellar structure is important in maintaining trend in hardness





Conclusions

- As-processed ARB material has similar morphology, chemistry as PVD, but different interfacial structure
- Density of interfaces <u>AND</u> interfacial structure play a role in determining hardness
 - Example: twinning in Cu at the {112}Cu//{112}Nb interface
 - Higher strength, no twinning in Cu in the {111}Cu//{110}Nb interface
- Need to understand effects of processing history to predict the effects on the interfaces we produce:
 - Amount of strain
 - Strain Path
 - Annealing